

# 4H-SiC Schottky barrier diodes as radiation detectors: A role of Schottky contact area

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## ABSTRACT

Large-area SiC Schottky barrier diodes can significantly improve the sensitivity in radiation detection due to the increased interacting SiC volume. In this work, we tested a large SiC detector with an area of  $1 \times 1 \text{ cm}^2$ . Extensive electrical characterization was performed at temperatures ranging from 150 K to 390 K, demonstrating the impact of barrier inhomogeneities on the electrical performance of the diode. Forward current-voltage (*I-V*) measurements of the diodes revealed two distinct regions caused by Schottky barrier inhomogeneity present throughout the entire temperature range. The barrier heights in the low- and high-current forward voltage regions were extracted from Richardson plots corrected for the Gaussian distribution of barrier heights, yielding values of 1.52 eV and 1.79 eV, respectively. Deep-level transient spectroscopy (DLTS) revealed only one deep-level defect,  $Z_{1/2}$ , with an activation energy for electron emission of 0.67 eV, which was assigned to the known carbon vacancy. The DLTS study showed no correlation between electrically active defects and barrier inhomogeneity. An excellent energy resolution of 3.2 % was measured using a large area  $^{241}\text{Am}$  radiation source, consistent with values for small area SiC detectors that exhibited no barrier height inhomogeneities. The impact of temperature on the alpha particle radiation response was determined within a temperature range of 200 K to 390 K.

## 1. Introduction

Silicon carbide (SiC) is a wide bandgap semiconductor with several polytypes, the best known of which are 3C, 4H, and 6H. Due to its various interesting properties, such as large critical electric field, high thermal conductivity, high electron saturation velocity, chemical inertness, and radiation hardness, SiC has attracted great interest as a promising material for numerous applications in quantum technology, power electronics, and radiation detection [1–9]. In particular, of all the polytypes, 4H-SiC is ideally suited for radiation detection applications in harsh environments due to its radiation-hardness [10,11].

Among the 4H-SiC-based devices utilized for radiation detection applications, the most widely used are *pin* diodes [12], metal-oxide-semiconductor (MOS) devices [13], and Schottky barrier diodes (SBDs) [9,11,14–19]. While being nearly the simplest electronic device, SBDs have been the most researched and used in recent years. A schematic of a typical n-type 4H-SiC SBD used for radiation detection is shown in Fig. 1.

In addition to the metallization used for the Schottky barrier diode, i.

e. Ni, Ti, Mo, geometrical parameters like the contact area and the thickness of the epitaxial layer are crucial for the sensitivity of SBD radiation detectors. The commonly reported values for the thickness of SiC epitaxial layers are a few tenths of micrometers. Recently, 4H-SiC epitaxial layers with thicknesses up to 250  $\mu\text{m}$  used for radiation detection applications have been reported [16,20].

The trend toward increasing the interacting SiC volume is supported by the development of larger area substrates, which now reach 8 in. [21]. Typical values for Schottky contact areas range from 1 to 20  $\text{mm}^2$  [9,11,14–19]. Most studies, reporting on radiation applications, use SiC SBDs with an area of about 15  $\text{mm}^2$ . Recently, studies on large area Schottky contacts have been reported. Liu et al. [22] have made significant progress with the largest reported area of 1  $\text{cm}^2$  or 4  $\text{cm}^2$  with parallel connection of four 1  $\text{cm}^2$  diodes [23]. Although it would be desirable for radiation applications to increase the Schottky contact area as much as possible, we are still limited in this regard because the contact area strongly affects the electrical properties of the SBDs.

Increasing the Schottky contact area can lead to a higher probability that the metal-semiconductor interface will be affected by surface

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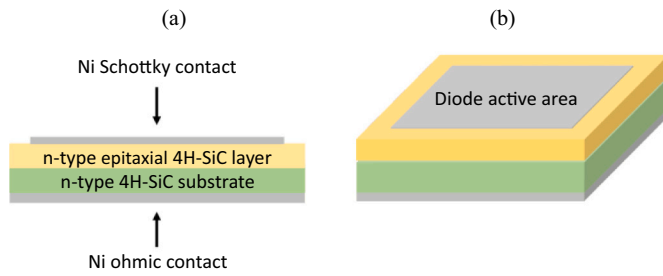


Fig. 1. Schematic of the Schottky barrier diode (a) cross-section and (b) three-dimensional view.

defects [24–26] or other parasitic effects such as doping inhomogeneity [26]. This leads to the formation of barrier height inhomogeneities in SiC SBDs that have been observed to impact the electrical performance and lead to temperature variations of the ideality factor and Schottky barrier height derived from the pure thermionic emission model [27]. The local effects and inhomogeneity at the metal-semiconductor interface decrease the Schottky barrier height and increase the ideality factor, causing the reverse saturation currents of the diode to increase [24–26,28]. Apart from the increase in dark current, the defects leading to barrier inhomogeneity may be electrically active and further degrade the performance of the detector [25,29,30]. However, in some cases, no correlation between electrically active defects and barrier inhomogeneities has been observed [24,31].

In this work, we fabricated a 4H-SiC SBD with one of the largest Schottky contact areas of  $1 \text{ cm}^2$ . The quality of the SBD was comprehensively investigated using temperature dependent current-voltage ( $I$ - $V$ - $T$ ) and capacitance-voltage ( $C$ - $V$ - $T$ ) measurements, as well as deep-level transient spectroscopy (DLTS) measurements. In addition, the radiation response to alpha particles was investigated in a wide temperature range.

## 2. Experimental details

We fabricated and characterized an SBD with a large area of  $1 \times 1 \text{ cm}^2$  on a  $25 \text{ }\mu\text{m}$  thick n-type nitrogen-doped 4H-SiC epitaxial layer. The SiC epitaxial layers were grown by chemical vapor deposition on an  $8^\circ$  off-cut silicon face of a  $350 \text{ }\mu\text{m}$  thick 4H-SiC (0001) wafer without a buffer layer. Ohmic contacts were formed on the backside of the SiC substrate by nickel sintering at  $950^\circ\text{C}$  in an Ar atmosphere. The surface was protected during the high temperature treatment for ohmic contact formation. The SBDs were formed by thermal evaporation of nickel with a thickness of  $100 \text{ nm}$  through a metal mask. The Schottky electrode was not annealed.

The quality of the fabricated large area SBDs was comprehensively evaluated by temperature-dependent current-voltage ( $I$ - $V$ - $T$ ) and capacitance-voltage ( $C$ - $V$ - $T$ ) measurements using a Keithley 4200 SCS (Keithley Instruments, Cleveland, OH, USA). Electrically active defects were characterized by deep-level transient spectroscopy (DLTS). DLTS measurements were performed in the temperature range of  $100$  to  $390 \text{ K}$ . The temperature ramp rate was  $2 \text{ K/min}$ . Capacitance transients were measured using a Boonton (Boonton Electronics, Parsippany, NJ, USA) 7200 capacitance meter with a  $30 \text{ mV}$ ,  $1 \text{ MHz}$  sinusoidal signal.

The radiation response of 4H-SiC SBDs to alpha particles was measured using a  $^{241}\text{Am}$  large area source (active area radius =  $25 \text{ mm}$ ,  $A = 3.4 \text{ kBq}$ ). The measurement system for radiation detection consisted of a charge-sensitive preamplifier (CREMAT CR-110), a Gaussian shaping amplifier (CREMAT CR-200-1 s), a multichannel analyzer (AMPTTEK MCA 8000D), and a laptop. To minimize the electronic noise, the system was operated with a battery power supply. A DC/DC converter (XP Power CA05P-5), also battery powered, was used to reversely bias the detector to  $100 \text{ V}$ . The shaping time was  $1 \text{ s}$ . Radiation response was measured at temperatures from  $200 \text{ K}$  to  $390 \text{ K}$  in a cryostat system.

## 3. Results and discussion

### 3.1. Impact of area size on electrical characteristics of SBDs

The presence of barrier height inhomogeneity in the large area SBD was confirmed by comparing the forward  $I$ - $V$  curves with diodes of  $1 \times 1 \text{ mm}^2$  and  $3 \times 3 \text{ mm}^2$  area, as shown in Fig. 2. The  $I$ - $V$  curve of the large area SBD exhibits two distinct regions in the low-current and high-current region attributed to the presence of two different Schottky barrier heights forming a parallel diode connection. The saturation current density of SBD using a pure thermionic emission model is given as follows [27]:

$$I_s = AA^* T^2 \exp\left(-\frac{q\phi_B}{kT}\right), \quad (1)$$

where  $A$  is the diode area,  $A^*$  is the Richardson constant with a value of  $146 \text{ A cm}^{-2} \text{ K}^{-2}$  for SiC,  $T$  is the temperature,  $q$  is the elementary charge,  $k$  is the Boltzmann constant, and  $\phi_B$  is the zero bias barrier height. The zero bias barrier height can be calculated as follows:

$$\phi_B = \frac{kT}{q} \ln \frac{AA^* T^2}{I_s}. \quad (2)$$

A comparison of the barrier height derived from (2) and the ideality factor of the diodes from Fig. 2 is given in Table 1.

The series resistance of a large-area SBD is  $3 \text{ }\Omega$  determined from the high-current region. The series resistance of the devices with the area of  $1 \times 1 \text{ mm}^2$  and  $3 \times 3 \text{ mm}^2$  is extracted to values of  $1.2 \text{ k}\Omega$  and  $25 \text{ }\Omega$ , respectively. The series resistance is seen to impact the electrical characteristics in the high-current region dominantly for the small-area devices. The nitrogen doping of the epitaxial layers of  $\sim 1.5 \times 10^{14} \text{ cm}^{-3}$  was determined from the  $C$ - $V$  measurement at room temperature.

### 3.2. Analysis of Schottky barrier height inhomogeneities

To analyze the impact of Schottky barrier height inhomogeneities in the large-area SBD, the diode was electrically characterized at temperatures from  $150 \text{ K}$  to  $390 \text{ K}$ . The forward  $I$ - $V$ - $T$  measurement of the diodes revealed that two distinct regions exist over the entire temperature range, as shown in Fig. 3. The saturation current density of the Schottky barrier dominates the low-current region and determines the reverse-bias leakage current down to  $\sim 40 \text{ V}$ , as shown in Fig. 3b for the reverse bias measurements at temperatures from  $200 \text{ K}$  to  $390 \text{ K}$ . The temperature dependence of the leakage current after  $\sim 60 \text{ V}$  reverse bias indicates the impact of tunneling mechanisms on the diode current [25,27]. Other mechanisms, such as generation-recombination

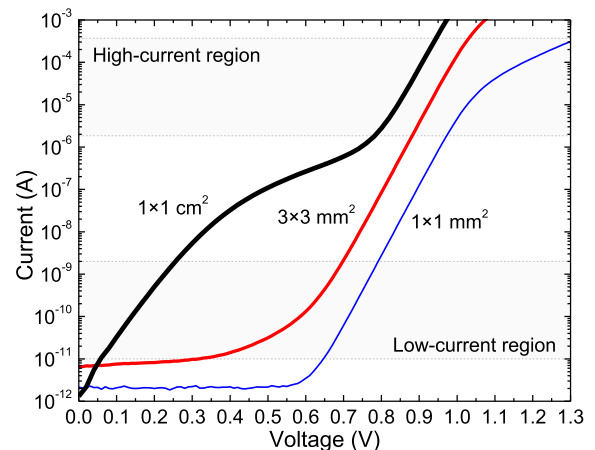
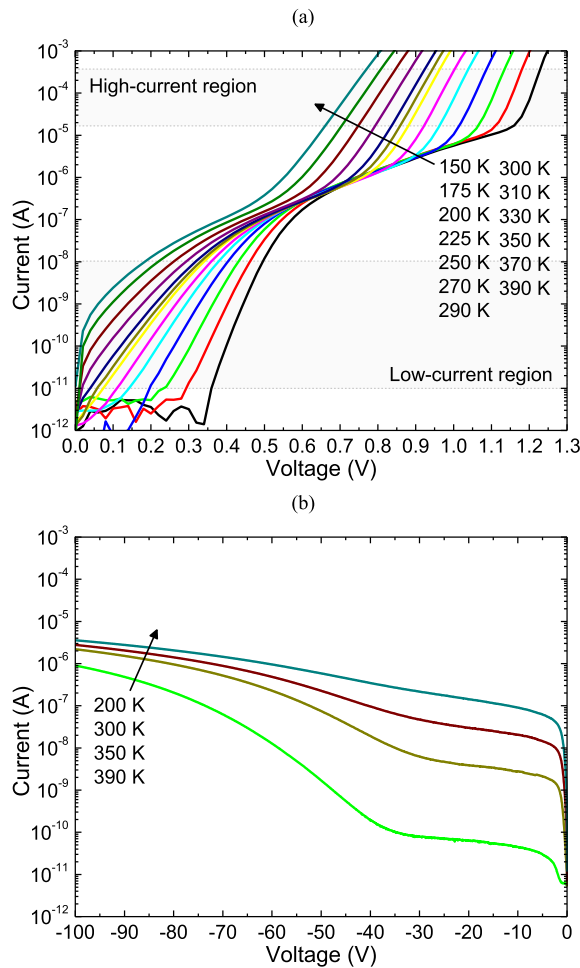


Fig. 2. Forward current-voltage characteristics of SBD with area of  $1 \times 1 \text{ mm}^2$ ,  $3 \times 3 \text{ mm}^2$  and  $1 \times 1 \text{ cm}^2$  measured at room temperature.

**Table 1**  
Barrier height,  $\phi_B$ , and ideality factor,  $n$ , of SBD with different diode area at room temperature.

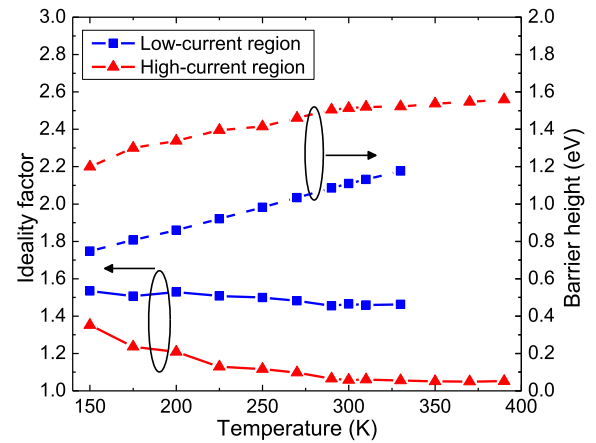
Diode area	Current region	$\phi_B$ (eV)	Ideality factor ( $n$ )
$1 \times 1 \text{ mm}^2$	–	1.59	1.01
$3 \times 3 \text{ mm}^2$	–	1.55	1.03
$1 \times 1 \text{ cm}^2$	Low-current	1.11	1.46
$1 \times 1 \text{ cm}^2$	High-current	1.51	1.06



**Fig. 3.** Current-voltage characteristics of a large  $1 \times 1 \text{ cm}^2$  SBD measured at (a) forward bias at temperatures from 150 K to 390 K (b) reverse bias down to 100 V at temperatures from 200 K to 390 K.

processes assisted by defects or trap-assisted tunneling, can also play a role on the observed temperature behavior of the leakage current [27].

The height of the Schottky barrier was determined using (2) for both saturation current densities in the low-current and high-current region for temperatures from 150 K to 330 K and for temperatures from 150 K to 390 K, respectively. For both regions, the height of the Schottky barrier increases with increasing temperature, as shown in Fig. 4. The ideality factor is plotted in the same graph as a function of the measured temperature. The ideality factor of the SBD in the high-current region is lower than the ideality factor of the SBD in the low-current region. This indicates the existence of charge transport mechanisms other than thermionic emission in the low-current region, which can include tunneling or generation-recombination mechanisms [25]. A higher ideality factor, as seen in the low-current region, could also be caused by inhomogeneous variations of the lateral  $\phi_B$  [25,32,33]. These mechanisms can affect the extraction of the ideality factor and the barrier



**Fig. 4.** Ideality factor and barrier height at low- and high-current regions as a function of measurement temperature.

height from the linear part of the semi-logarithmic  $I$ - $V$  curve in the low-current region, and the values for temperatures above 330 K were not included in the analysis.

Eq. (1) can be written as:

$$\ln\left(\frac{I_s}{T^2}\right) = \ln(AA^*) - \frac{q\phi_B}{kT}, \quad (3)$$

and the plot of  $\ln(I_s/T^2)$  as a function of  $1/T$ , called the Richardson plot, can be used to extract  $\phi_B$ . The Richardson plot was used to extract the barrier heights in the low- and high-current regions, yielding values of 0.39 eV and 0.99 eV, respectively. The Richardson plot method is not able to determine the exact value of the barrier height due to the barrier height inhomogeneities, resulting in a large discrepancy between the extracted values and the values reported in the literature [34,35].

A model of barrier height that assumes Gaussian spatial distribution of barrier heights across the interface can better explain the temperature dependence of  $\phi_B$  and allows the extraction of the apparent barrier height,  $\phi_{B,ap}$  [36]. The standard deviation,  $\sigma$ , and the mean value of the Gaussian distribution of the barrier height,  $\overline{\phi_B}$ , are determined from the plot of the barrier height as a function of temperature. The values of  $\sigma$  for the low-current and high-current regions are 0.143 V and 0.124 V, respectively. Assuming a Gaussian distribution of barrier heights, Eq. (1) can be rewritten as follows [36]:

$$I_s = AA^* T^2 \exp\left[-\frac{q\phi_{B,ap}}{kT} + \frac{q^2\sigma^2}{2k^2T^2}\right], \quad (4)$$

where the modification for the Richardson plot is given as follows:

$$\ln\left(\frac{I_s}{T^2}\right) - \frac{q^2\sigma^2}{2k^2T^2} = \ln(AA^*) - \frac{q\phi_{B,ap}}{kT}. \quad (5)$$

The modified Richardson plots are shown in Fig. 5 for both the low- and high-current regions. The apparent barrier heights of 1.52 eV and 1.79 eV were calculated for the low- and high-current regions, respectively, and agree well with the values reported in the literature. The modified Richardson constant was  $155 \text{ A cm}^{-2} \text{ K}^{-2}$  for the barrier in the high-current region, assuming an area of  $1 \text{ cm}^2$ , which agrees with the theoretical value.

### 3.3. Deep-level transient spectroscopy of large-area SBD

The as-grown large-area 4H-SiC SBD was characterized by deep-level transient spectroscopy (DLTS). The DLTS spectra for emission rates of 10 and  $20 \text{ s}^{-1}$  are shown in Fig. 6. It is evident that only one DLTS peak with a maximum at around 300 K, known as  $Z_{1/2}$ , is present in the spectra. The activation energy,  $E_a$ , for electron emission and the apparent

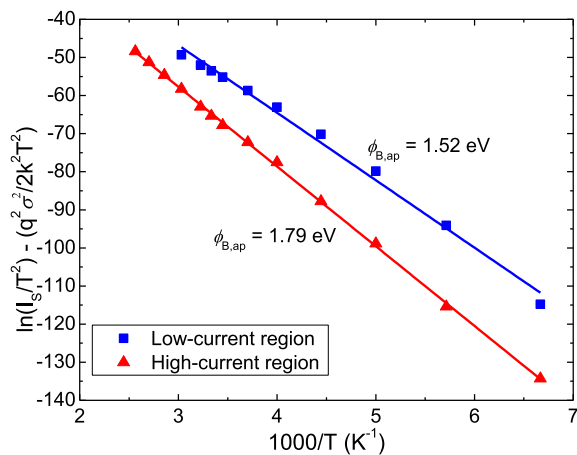


Fig. 5. Modified Richardson plot with the Gaussian distribution of barrier heights across the metal-semiconductor interface.

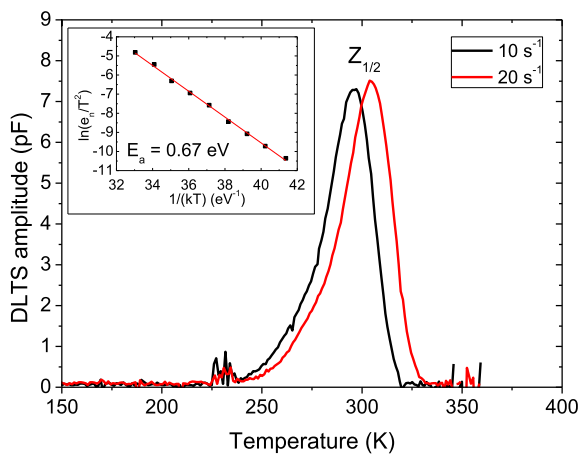


Fig. 6. DLTS spectra for the as-grown 4H-SiC SBD. Measurement settings are  $V_R = -10$  V,  $V_P = -0.1$  V,  $t_P = 0$  ms. Emission rates are  $10$  s $^{-1}$  and  $20$  s $^{-1}$ . Inset: Arrhenius plot of the  $T^2$ -corrected electron emission rate.

capture cross sections for the  $Z_{1/2}$  deep level were determined from the Arrhenius plot of the  $T^2$ -corrected electron emission rate, as shown in the inset of Fig. 6. The activation energy and apparent capture cross section of the  $Z_{1/2}$  deep level are  $E_C - 0.67$  eV and  $1.04 \times 10^{-14}$  cm $^2$ , respectively.

$Z_{1/2}$  is a well-known deep level defect, and it has already been assigned to the carbon vacancy ( $V_C$ ) [37–39].  $V_C$  is often referred to as a “lifetime killer” due to its detrimental effect on carrier lifetime [40]. It is one of the most important and dominant defects in 4H-SiC material. It introduces the deep level defect ( $Z_{1/2}$ ), which acts as a very efficient trap or recombination center for the charge carriers. A trap concentration of  $7.02 \times 10^{12}$  cm $^{-3}$  was calculated from DLTS measurements.

No correlation was found between the electrically active defects and barrier inhomogeneity in the DLTS study.

### 3.4. Radiation response of large-area SBD

Irradiations of 4H-SiC SBDs with alpha particles of different energy were performed at a range of temperatures between 200 K and 390 K under a vacuum of less than 0.1 mbar. The distance between the source and the detector was kept at 5 mm. The radiation response to the alpha source  $^{241}\text{Am}$  ( $E_{\text{max}} = 5486$  keV) is shown in Fig. 7. The energy resolution for  $^{241}\text{Am}$  was 3.2 % at 300 K and is consistent with the values of 3 % reported in previous studies where the measurements were

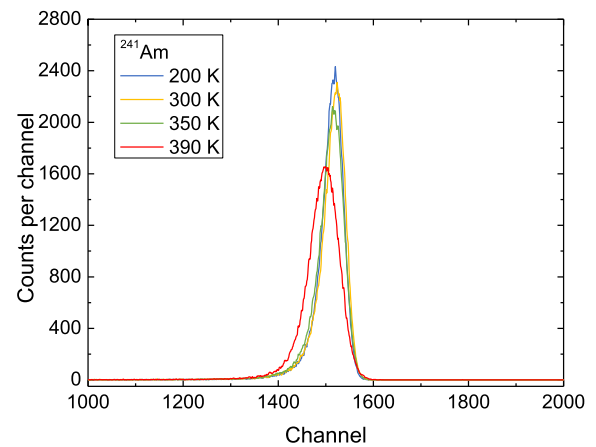


Fig. 7. Radiation response of 4H-SiC detectors with surface area of  $1 \times 1$  cm $^2$  to  $^{241}\text{Am}$  alpha particles at 200 K, 300 K, 350 K and 390 K.

performed on small area SiC SBDs in vacuum [41].

Since the saturation current density of the Schottky barrier dominates the low-current region and determines the reverse-bias leakage current, as shown in Fig. 3b for temperatures from 200 K to 390 K, the impact of temperature on the radiation response of the detector was measured. The radiation response for  $^{241}\text{Am}$  was determined at temperatures from 200 K to 390 K, as shown in Fig. 7. The energy resolutions for the radiation response of  $^{241}\text{Am}$  at temperatures of 200 K, 300 K, 350 K, and 390 K are 3.2 %, 3.2 %, 3.5 %, and 4.9 %, respectively. Although the leakage current is high at an operating reverse bias voltage of 100 V and increases with temperature, the energy resolution was not significantly affected by operation at elevated temperatures.

## 4. Conclusions

Extensive electrical characterization of a  $1 \times 1$  cm $^2$  SBD showed the variation of the ideality factor and Schottky barrier height with temperature. Two different Schottky barriers were identified to affect the forward-bias current in either the low-current or high-current regions. This was explained by an inhomogeneity of the Schottky barrier height at the metal-semiconductor interface. The barrier height inhomogeneity was not readily observed for devices with smaller areas. This is due to the statistical nature of the formation of surface defects or possible doping inhomogeneity, which is thought to lead to the formation of barrier inhomogeneity. Modified Richardson plots were used to determine the apparent barrier heights, assuming a Gaussian variation in barrier inhomogeneity. The apparent barrier heights of 1.52 eV and 1.79 eV were extracted for the low- and high-current regions, respectively. The DLTS study revealed no correlation between barrier height inhomogeneity and electrically active defects. Only one deep-level defect,  $Z_{1/2}$ , was assigned to the known carbon vacancy with an activation energy for electron emission of 0.67 eV. The radiation response of large area detectors to alpha particles confirmed that the larger Schottky area increases the sensitivity of the detector and that the inhomogeneity of the barrier height does not significantly affect the energy resolution even when the diode is operated at elevated temperatures.

### CRedit authorship contribution statement

**Ivana Capan:** Conceptualization, Data curation, Formal analysis, Funding acquisition, Investigation, Methodology, Project administration, Resources, Supervision, Validation, Visualization, Writing – original draft, Writing – review & editing. **Robert Bernat:** Data curation, Formal analysis, Investigation, Visualization, Writing – original draft, Writing – review & editing. **Takahiro Makino:** Data curation, Formal analysis, Investigation, Resources, Validation, Writing – review &

editing. **Tihomir Knežević:** Data curation, Formal analysis, Investigation, Visualization, Writing – original draft, Writing – review & editing.

### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

### Data availability

Data will be made available on request.

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